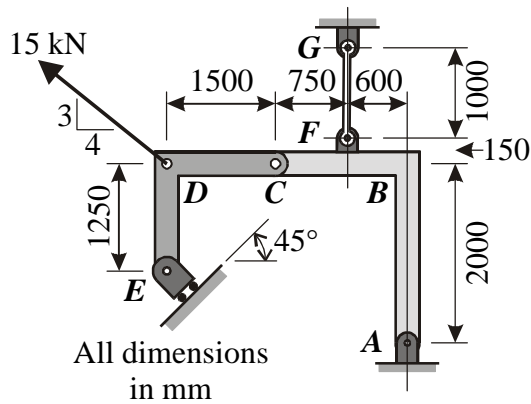


Question 1:**Given:**

$$L_{AB} = 2000 \cdot \text{mm} \quad L_{BC} = 1350 \cdot \text{mm}$$

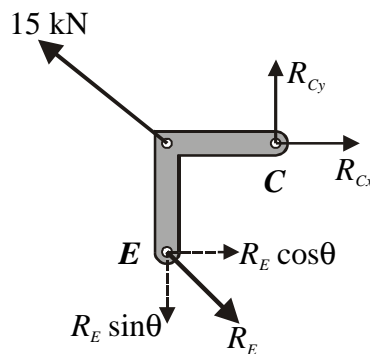
$$L_{CD} = 1500 \cdot \text{mm} \quad L_{DE} = 1250 \cdot \text{mm}$$

$$L_{BF} = 600 \cdot \text{mm} \quad \theta_E = 45 \cdot \text{deg}$$

$$F_D = 15 \cdot \text{kN}$$

$$d_C = 16 \cdot \text{mm} \quad \tau_u = 80 \cdot \text{MPa}$$

$$\sigma_{\text{all}} = 175 \cdot \text{MPa}$$

FBD of Member CDE:

$$\Sigma M_C = 0$$

$$-\left(\frac{3}{5} \cdot F_D\right) \cdot (L_{CD}) + (R_E \cdot \sin(\theta_E)) \cdot (L_{CD}) + (R_E \cdot \cos(\theta_E)) \cdot (L_{DE}) = 0$$

$$R_E = \frac{3}{5} \cdot F_D \cdot \frac{L_{CD}}{\sin(\theta_E) \cdot L_{CD} + \cos(\theta_E) \cdot L_{DE}}$$

$$R_E = 6.943 \text{ kN} \quad (\text{acting in direction shown})$$

$$\Sigma F_x = 0 \quad -\left(\frac{4}{5} \cdot F_D\right) + R_{Cx} + R_E \cdot \cos(\theta_E) = 0$$

$$R_{Cx} = \frac{4}{5} \cdot F_D - R_E \cdot \cos(\theta_E) \quad R_{Cx} = 7.091 \text{ kN} \quad (\text{acting to right})$$

$$\Sigma F_y = 0 \quad \left(\frac{3}{5} \cdot F_D\right) + R_{Cy} - R_E \cdot \sin(\theta_E) = 0$$

$$R_{Cy} = \frac{3}{5} \cdot F_D + R_E \cdot \sin(\theta_E) \quad R_{Cy} = -4.091 \text{ kN} \quad (\text{acting downward})$$

(a) Factor of safety in Pin at Point C

- Resultant shear force in pin (single shear): $V_C = \sqrt{R_{Cx}^2 + R_{Cy}^2} \quad V_C = 8.186 \text{ kN}$

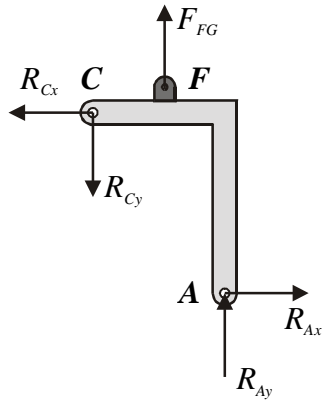
- Cross-sectional area: $A_C = \frac{\pi}{4} \cdot d_C^2 \quad A_C = 201.062 \times 10^{-6} \text{ m}^2$

- Ultimate shear strength: $V_u = \tau_u \cdot A_C \quad V_u = 16.085 \text{ kN}$

- Factor of safety: $\text{FOS} = \frac{V_u}{V_C} \quad \text{FOS} = 1.965$

(b) Required size of Member FG

FBD of Member ABC:



$$\Sigma M_A = 0$$

$$(R_{Cx}) \cdot (L_{AB}) + (R_{Cy}) \cdot (L_{BC}) - (F_{FG}) \cdot (L_{BF}) = 0$$

$$F_{FG} = \frac{R_{Cx} \cdot L_{AB} + R_{Cy} \cdot L_{BC}}{L_{BF}} \quad F_{FG} = 14.432 \text{ kN}$$

(in tension)

$$\Sigma F_x = 0 \quad -R_{Cx} + R_{Ax} = 0 \quad R_{Ax} = R_{Cx}$$

$$R_{Ax} = 7.091 \text{ kN}$$

$$\Sigma F_y = 0 \quad -R_{Cy} + F_{FG} + R_{Ay} = 0$$

$$R_{Ay} = R_{Cy} - F_{FG} \quad R_{Ay} = -18.523 \text{ kN}$$

(acting downward)

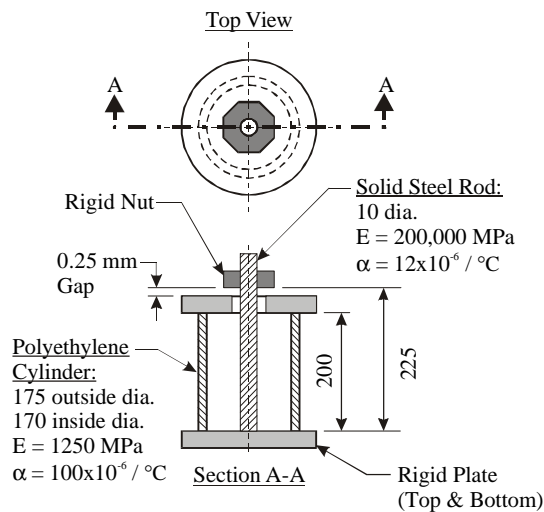
Required size of Member FG:

$$A_{\text{req}} = \frac{|F_{FG}|}{\sigma_{\text{all}}} \quad A_{\text{req}} = 82.468 \times 10^{-6} \text{ m}^2$$

$$b = \sqrt{A_{\text{req}}} \quad b = 9.081 \text{ mm}$$

$$\text{MPa} := 10^6 \cdot \text{Pa}$$

$$\text{kN} := 10^3 \cdot \text{N}$$



Input data: $\Delta T := 80 \cdot \text{deg}$

$$\delta_{\text{gap}} := 0.25 \cdot \text{mm}$$

- Cylinder: $L_c := 200 \cdot \text{mm}$

$$d_o := 175 \cdot \text{mm} \quad d_i := 170 \cdot \text{mm}$$

$$E_c := 1250 \cdot \text{MPa}$$

$$\alpha_c := \frac{100 \cdot 10^{-6}}{\text{deg}}$$

- Rod: $L_r := 225 \cdot \text{mm}$

$$d_r := 10 \cdot \text{mm}$$

$$E_r := 200000 \cdot \text{MPa}$$

$$\alpha_r := \frac{12 \cdot 10^{-6}}{\text{deg}}$$

Thermal expansion:

$$\delta_{c_T} := \alpha_c \cdot \Delta T \cdot L_c \quad \delta_{c_T} = 1.6 \text{ mm}$$

$$\delta_{r_T} := \alpha_r \cdot \Delta T \cdot L_r \quad \delta_{r_T} = 0.22 \text{ mm}$$

Equilibrium:

$$\Sigma F_y = 0 \quad P_r - P_c = 0$$

$$P_r = P_c$$

Cross Sectional Areas:

$$A_c := \frac{\pi}{4} \cdot (d_o^2 - d_i^2) \quad A_c = 1354.81 \text{ mm}^2$$

$$A_r := \frac{\pi}{4} \cdot d_r^2 \quad A_r = 78.54 \text{ mm}^2$$

Axial deformation:

$$\delta_{c_P} = \frac{(-P_c) \cdot L_c}{A_c \cdot E_c} = \frac{(-P_r) \cdot L_c}{A_c \cdot E_c}$$

$$\frac{L_c}{A_c \cdot E_c} = 118.1 \times 10^{-9} \frac{\text{m}}{\text{N}}$$

$$\delta_{r_P} = \frac{P_r \cdot L_r}{A_r \cdot E_r}$$

$$\frac{L_r}{A_r \cdot E_r} = 14.32 \times 10^{-9} \frac{\text{m}}{\text{N}}$$

Geometric compatibility:

$$\delta_{c_P} + \delta_{c_T} - \delta_{\text{gap}} = \delta_{r_P} + \delta_{r_T}$$

$$\frac{(-P_r) \cdot L_c}{A_c \cdot E_c} + \delta_{c_T} - \delta_{\text{gap}} = \frac{P_r \cdot L_r}{A_r \cdot E_r} + \delta_{r_T}$$

$$P_r := \frac{-\delta_{r_T} + \delta_{c_T} - \delta_{\text{gap}}}{L_r \cdot A_c \cdot E_c + L_c \cdot A_r \cdot E_r} \cdot A_r \cdot E_r \cdot A_c \cdot E_c$$

$$P_r = 8.564 \text{ kN}$$

$$\sigma_r := \frac{P_r}{A_r} \quad \sigma_r = 109.03 \text{ MPa}$$

Deformations and final lengths:

$$P_c := P_r$$

$$\sigma_c := \frac{-P_c}{A_c} \quad \sigma_c = -6.32 \text{ MPa}$$

$$\delta_{c_P} := \frac{(-P_c) \cdot L_c}{A_c \cdot E_c}$$

$$\delta_{c_P} = -1.011 \text{ mm}$$

$$L_{c_final} := L_c + \delta_{c_P} + \delta_{c_T}$$

$$L_{c_final} = 200.589 \text{ mm}$$

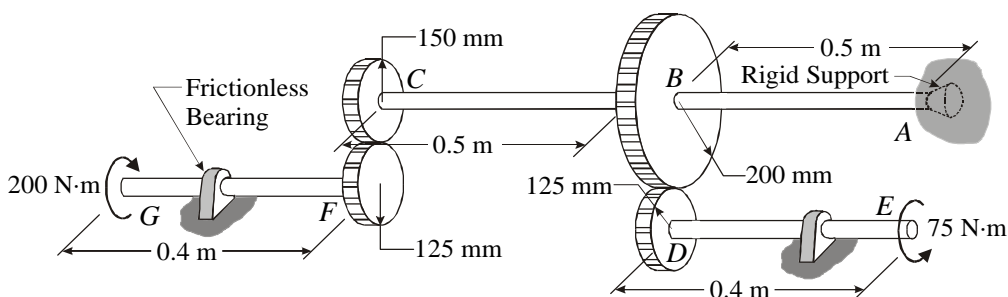
$$\delta_{r_P} := \frac{(P_r) \cdot L_r}{A_r \cdot E_r}$$

$$\delta_{r_P} = 0.123 \text{ mm}$$

$$L_{r_final} := L_r + \delta_{r_P} + \delta_{r_T}$$

$$L_{r_final} = 225.339 \text{ mm}$$

$$(\delta_{c_P} + \delta_{c_T}) - (\delta_{r_P} + \delta_{r_T}) = 0.25 \text{ mm}$$

Question 3:

Given: $d = 40 \cdot \text{mm}$

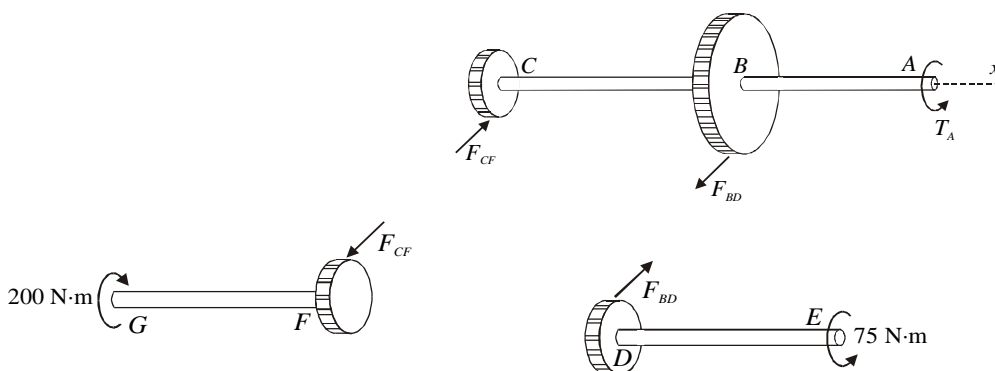
$$L_{AB} = 500 \cdot \text{mm} \quad L_{BC} = 500 \cdot \text{mm} \quad L_{DE} = 400 \cdot \text{mm} \quad L_{FG} = 400 \cdot \text{mm}$$

$$c_B = 200 \cdot \text{mm} \quad c_C = 150 \cdot \text{mm} \quad c_D = 125 \cdot \text{mm} \quad c_F = 125 \cdot \text{mm}$$

$$T_E = 75 \cdot \text{N} \cdot \text{m} \quad T_G = 200 \cdot \text{N} \cdot \text{m} \quad \underline{\underline{G = 77000 \cdot \text{MPa}}}$$

Solution:

FBD's: (Neglecting all reactions that don't produce moments about x-axis)



Shaft DE:

$$\Sigma M_x = 0 \quad T_E - (F_{BD} \cdot c_D) = 0 \quad F_{BD} = \frac{T_E}{c_D} \quad F_{BD} = 600 \text{ N} \quad \text{in direction shown}$$

Shaft FG:

$$\Sigma M_x = 0 \quad -T_G + (F_{CF} \cdot c_F) = 0 \quad F_{CF} = \frac{T_G}{c_F} \quad F_{CF} = 1600 \text{ N} \quad \text{in direction shown}$$

Shaft ABC:

$$\Sigma M_x = 0 \quad (F_{CF} \cdot c_C) - (F_{BD} \cdot c_B) + T_A = 0 \quad T_A = -F_{CF} \cdot c_C + F_{BD} \cdot c_B$$

$$T_A = -120 \text{ N} \cdot \text{m} \quad \curvearrowright$$

Part (a): Shear stress in shaft AB

$$d = 40 \text{ mm}$$

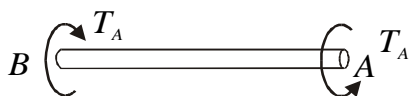
- Polar moment of inertia (all shafts): $J = \frac{\pi}{2} \cdot \left(\frac{d}{2}\right)^4$ $J = 251.33 \times 10^{-9} \text{ m}^4$

- Shear stress: $\tau_{AB} = \frac{|T_A| \cdot \left(\frac{d}{2}\right)}{J}$ $\tau_{AB} = 9.55 \text{ MPa}$

Part (b): Angle of twist at Point E

$$\phi_A = 0 \cdot \text{rad} \quad (\text{rigid support})$$

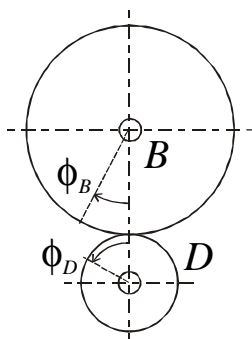
- Shaft AB:



$$\phi_{BA} = \frac{-T_A \cdot L_{AB}}{J \cdot G} \quad \phi_{BA} = 3.1 \times 10^{-3} \text{ rad} \quad \curvearrowright$$

$$\phi_B = \phi_{BA} + \phi_A \quad \phi_B = 3.1 \times 10^{-3} \text{ rad} \quad \curvearrowright$$

- Angle of twist of gear D: Same arc length travelled by both gears

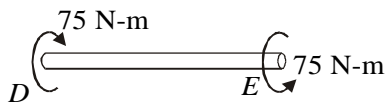


$$\phi_B \cdot c_B = -\phi_D \cdot c_D$$

$$\phi_D = -\phi_B \cdot \frac{c_B}{c_D} \quad \phi_D = -4.96 \times 10^{-3} \text{ rad} \quad \curvearrowright$$

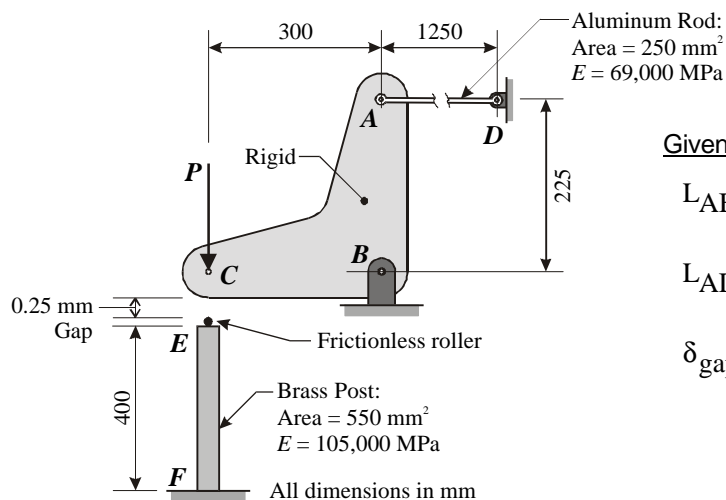
Looking from right
to left

- Shaft DE:



$$\phi_{ED} = \frac{T_E \cdot L_{DE}}{J \cdot G} \quad \phi_{ED} = 1.55 \times 10^{-3} \text{ rad} \quad \curvearrowright$$

$$\phi_E = \phi_{ED} + \phi_D \quad \phi_E = -3.41 \times 10^{-3} \text{ rad} \quad \curvearrowright$$

Question 4:**Given:**

$$L_{AB} = 225 \cdot \text{mm} \quad L_{BC} = 300 \cdot \text{mm}$$

$$L_{AD} = 1250 \cdot \text{mm} \quad L_{EF} = 400 \cdot \text{mm}$$

$$\delta_{\text{gap}} = 0.25 \cdot \text{mm}$$

- Aluminum rod: $A_{\text{al}} = 250 \cdot \text{mm}^2$ $E_{\text{al}} = 69000 \cdot \text{MPa}$

- Brass post: $A_{\text{br}} = 550 \cdot \text{mm}^2$ $E_{\text{br}} = 105000 \cdot \text{MPa}$ $\epsilon_{\text{br}} = -0.0014$

Solution:

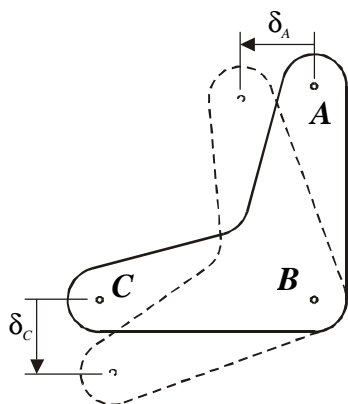
- Axial deformation of the brass post: $\delta_{EF} = \epsilon_{\text{br}} \cdot L_{EF}$ $\delta_{EF} = -560 \times 10^{-6} \text{ m}$

Since $\delta_F = 0 \cdot \text{m}$ $\delta_E = \delta_{EF} + \delta_F$ $\delta_E = -560 \times 10^{-6} \text{ m}$

- Total vertical displacement of Point C:

$$\delta_C = \delta_E - \delta_{\text{gap}} \quad \delta_C = -810 \times 10^{-6} \text{ m}$$

- Horizontal displacement of Point A: (small displacement theory)



Similar triangles:

$$\frac{\delta_A}{L_{AB}} = \frac{-\delta_C}{L_{BC}}$$

$$\delta_A = \frac{-\delta_C}{L_{BC}} \cdot L_{AB} \quad \delta_A = 607.5 \times 10^{-6} \text{ m}$$

(assume +ve to left)

- Axial deformation of aluminum rod: $\delta_D = 0 \cdot \text{m}$

$$\delta_{AD} = \delta_A - \delta_D \quad \delta_{AD} = 607.5 \times 10^{-6} \text{ m}$$

- Axial forces:

- Brass post (compression):

$$\delta_{EF} = \frac{(-F_{EF}) \cdot L_{EF}}{A_{br} \cdot E_{br}}$$

$$F_{EF} = \frac{-\delta_{EF}}{L_{EF}} \cdot A_{br} \cdot E_{br}$$

$$F_{EF} = 80.85 \times 10^3 \text{ N}$$

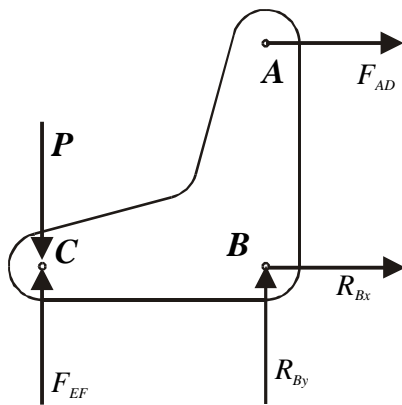
- Aluminum rod (tension)

$$\delta_A = \frac{F_{AD} \cdot L_{AD}}{A_{al} \cdot E_{al}}$$

$$F_{AD} = \frac{\delta_A}{L_{AD}} \cdot A_{al} \cdot E_{al}$$

$$F_{AD} = 8.383 \times 10^3 \text{ N}$$

- FBD of bracket ABC:



$$\Sigma M_B = 0 \quad \text{(+ve)}$$

$$(-F_{AD}) \cdot (L_{AB}) - (F_{EF}) \cdot (L_{BC}) + P \cdot (L_{BC}) = 0$$

$$P = \frac{F_{AD} \cdot L_{AB} + F_{EF} \cdot L_{BC}}{L_{BC}}$$

$$P = 87.138 \times 10^3 \text{ N} \quad (\text{in direction shown})$$